FELDMAN Z. A.

Novocaine (procaine) block in lead poisoning Klinicheskaya Meditsina 1947, 1

4434 In 45 cases of oliguria, lead colic and other forms of entero-gastric dyskinesia, infiltration of the left perirenal tissues with 60 ml 0.5 per cent processe gave gratifying results.

Van der Molen - Terwolde (SecVI)

SO: Section II Vol. 1² No. 7-12

TSEYTLIN, A.A.; FEL'DMAN, Z.D.; BUZBITSKIY, Ye.V.; DEKHTYAR, E.M.

CHECKER CONTRACTOR CONTRACTOR OF THE CONTRACTOR CONTRAC

Machine for making curvilinear reinforced concrete products. Suggested by A.A.TSeytlin, Z.D.Fel!dman, E.V.Buznitskii, E.M.Dekhtiar. Rats. i izobr. predl. v stroi. no.15:41-43 '60. (MIRA 13:9)

1. Po materialam Tekhnicheskogo upravleniya Ministerstva stroitel'stva USSR.

(Concrete panels)

KIRICHEMEO, T.F.; FEL'DMAN, E.G.

Record of trees and shrubs in the territory of the Veliko-Anadol'
Forest. Mauk.sap.Dnipr.un. 48:227-239 '55 (MIRA 10:11)

(Ol'ginka District—Trees) (Ol'ginka District—Shrubs)

SANDLER, N.I.; DOBRUSKINA, Sh.R.; ZAYKOV, S.T.; FEL DMAN, Z.M., ASNIS A.Ye.; NAZARENKO, A.N.

Converter low-alloys steel with niobium for welded structures. Avtom. svar. 17 no.2:43-48 F '64. (MTRA 17:9)

1. Ukrainskiy institut metallov (for Sandler, Dobruskina, Zaykov, Fel'dman). 2. Institut elektrosvarki im. Ye.O. Patona AN UkrSSR (for Asnis, Nazarenko).

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000412830

FELDMAN, Z. VA.
USSR/Microbiology -/Antibiosis and Symbiosis. Antibiotics.

Abs Jour

: Ref Zhur - Biol., No 5, 1958, 19433

Author

Feldman, 7. Ya.

Inst

Utilization of Antibiotics in Storing Lemon.

Title

Orig Pub

Tr. Leningr. tekhnol. in-t kholodiln. prom-sti, 1956, 10,

72-73

Abstract

Antibiotic preparations were obtained by the method of N.V. Novotelnov from dog-rose fruit and bran. Antibiotics from bran were obtained with and without fermentation. These preparations when used with ascorbic acid exert high bactericidal properties, inhibit development of brown spots on lemons, and prevent spoilage of fruit to a considerable degree when it is stored at 13-15° for a period of 3 months. Most active was an antibiotic obtained from bran after fermentation. In its presence Lemons were fully preserved at

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Senergiad kholodil nike Glavnoge upravleniga gastronomickenkikh bakaleynik mogeze

APPROVED FOR RELEASE: Monday, July 31, 2000 ... CIA-RDP86-00513R0004128

: Ref Zhur - Biol., No 5, 1958, 19433 Abs Jour

16-220 for a period of 25 months, while the majority of the control lemons became moldy after 10 days.

SHVARTS, K. [Svaros, K.]; FELDMANE, ...

Microscopic studies of the defects in alkali-halogenous crystals by the evaporation method. [zv. AN Latv.SSR no.9:57-59 '63.

(MIRA 16:12)

1. Institut fiziki AN Latviyskoy SSR.

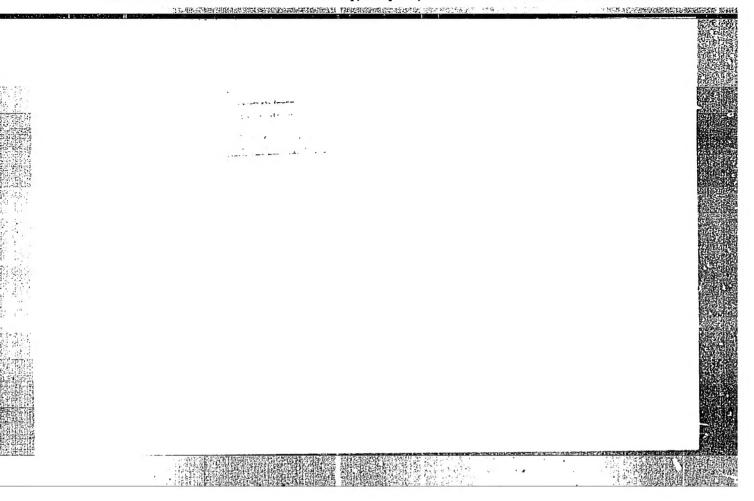
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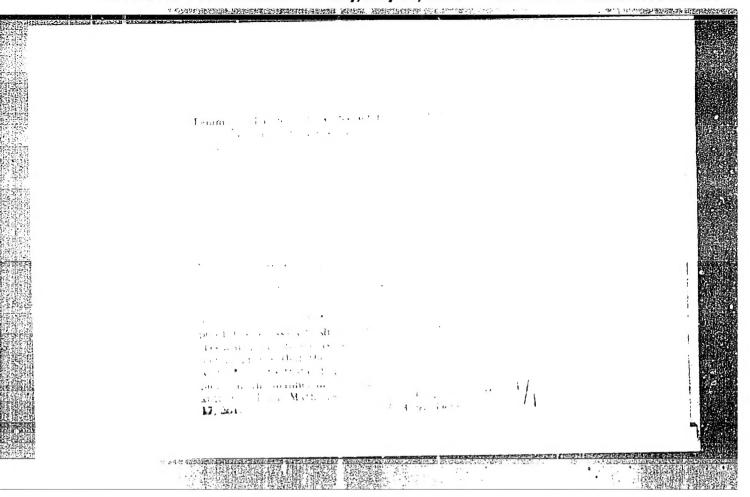
CIA-RDP86-00513R000412830

ACC NR: AP7005269 SOURCE CODE: UR/0371/66/000/006/0101/0102 AUTHOR: Kalnin', D. O.; Shavrts, K. K.; Feldmane, E. E. ORG: Physics Institute, AN Latvian SSR (Institut fiziki AN LatvSSR) TITLE: Dislocation density and radiation expansion in crystals SOURCE: AN LatSSR. Izvestiya. Seriya fizicheskikh i tekhnicheskikh nauk, no. 6. 1966, 101-102 cusatal crystal TOPIC TAGS: lithium fluoride, radiation expansion, dislocation, neutron irradiation, plantic deformation, engatal defect ABSTRACT: Radiation expansion and point defects in crystals were studied experimentally. LiF crystals (10 x 10 x 2 mm) grown in a 10^{-4} ton vacuum were used. Dislocation density, determined by FeCl₃ etching, was 10^4 cm⁻² for non-worked samples, and 10^6 cm⁻² after plastic deformation at 1000K. The samples were irradiated with doses of 4.10^{14} — 4.10^{17} neutrons/cm³. At low doses fractional volume expansion decreased slowly with increasing dislocation density; at high doses no effect was detected. The results indicate that an increase in dislocation density from 104 to 106 cm-2 has little effect on the radiational change in the volume in the range up to 5 x 1016 neutrons/cm3. This suggests that dislocations play an unimportant role in the crystal expansion. Orig. art. has: 1 figure. SUB CODE: 20/ SUBM DATE: none/ ATD PRESS: 5115 Card 1/1 UDC: none

FEL DMAN-RABAK, Tamara Petrovna; SURYGINA, E., red.; NEMCHENKO, I., tekin.red.

[Outdoor swimming pools] Otkrytye iskusstvennye basseiny dlia plavaniia. Kiev, Gos.isd-vo lit-ry po stroit. i arkhit. USSR. 1960. 161 p. (NIRA 13:12)

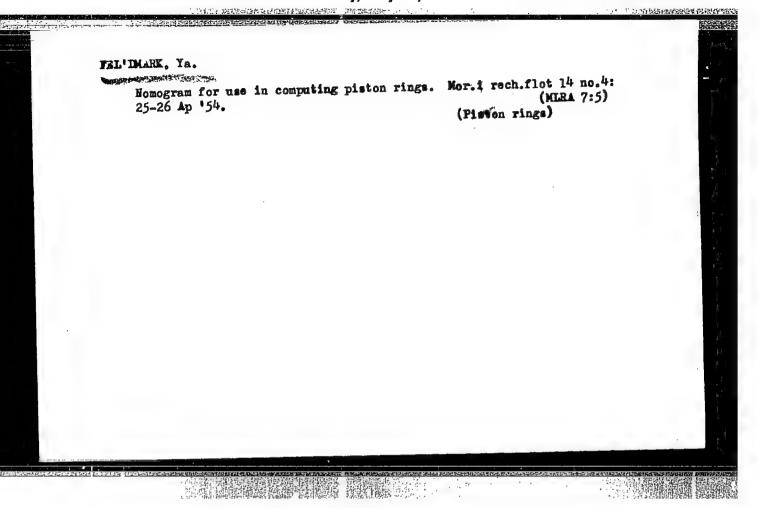




FELDMANN, L. (Budapest, V., Szerb u.23)

On linear difference equations with constant coeeficients. Periodica polytechn electr 3 no.3:247-257 '59.

1. Polytechnical University, Budapest.
(Difference equations)



FEL'DMUS, F.

Here we learn our trade. Mest.prom. i khud.promys. 4 no.4:
(MRA 16:10)
23 Ap '63.

1. Direktor Golitsynskogo uchebnogo kombinata, Moskovskoy obl.

EL' DSHAW, Fel'dshau, A.F. and Starokadomskiy, K. G. 65-1-14/14 AUTHORS: On a Source of Error During the Evaluation of Coals for Power Stations According to their Ash Content. (Ob TITLE: odnom istochnike oshibok pri otsenke energeticheskikh ugley po ikh zol'nosti). PERIODICAL: Khimiya i Tekhnologiya Topliv i Masel, 1958, No. 1, p. 72. (USSR). ABSTRACT:

The evaluation of coal on the basis of their ash content may lead to large errors when the mineral matter contains a considerable proportion of carbonates. Therefore, the best method of evaluation of coals for power generation is on the basis of their calorific value. The experiments were carried out by the Chemical Laboratory for Coal Investigations of the Lenin-Ugol' Trust of the Karagandaugol' Combine. A sample of coal was supplied by the No.120 Trust of Saranugol:- specific weight = 1.83, ash content = A = 38%, ash content of the dry mass As = 38.3%, Coal = 23.6%, calorific value Oa = 3210 ccal/kg (total fuel content OS = 5310 ccal/kg). It is concluded that the ash content decreased by 23.6% and a value of OS = 8390 ccal/kg is obtained which is near to the average value. the best method of evaluation of coals for power generat-

Card 1/1 Library of Congress. AVAILABLE:

INDEMBAUM, I.S.; PERSHIN, G.N., prof., nauchnyy rukovod.; SEMILETOVA, A., red.; FEL'DSHER, L., otv. za vypusk; SOYFERTIS, L., tekhn.red.

[Medicinal preparations: collection of annotations] Lekarstvennye preparaty: abornik annotatsii. Pod nauchn.rukovodstvom G.N.
Pershina. Sost. I.S.Indenbaum. Moskva, Kontora "Soiuzkhimfarmtorg," 1959. 332 p. (MIRA 13:3)

1. Russia (1923- U.S.S.R.) Glavnoye upravleniye meshrespublikanskogo meditsinakogo snabsheniya i sbyta. (DRUGS)

POLYAKOV, N.G., prof.; CHERIKOVSKAYA, T.Ya., kand. med. nauk; SIDORKOV, A.M., kand. farmatsevt. nauk; BELEN'KIY, Ye.Ye., kand. med. nauk; KUZ'MINA, K.K., provizor; VASIL'YEVA, S.F., provizor; POLYAKOV, N.G., prof., red.; FEL'DSHER, L.N., red.; KUCHERENKO, V.D., red.; CHULKOV, I.F., tekhn. red.

[Basic medicinal preparations and prepared drugs; a manual for physicians] Osnovnye lekarstvennye preparaty i gotovye formy; spravochnik dlia vrachei. Moskva, Medgiz, 1963. 359 p. (MIRA 17:2)



POCHKOV, N.G., prof.; CHERIKOVSKAYA, T.Ya., kand. med. nauk;
SIDORKOV, A.M., kand. farmatsevt. nauk; KUCHERENKO, V.D.,
provizor; KUZ'MINA, K.K., provizor; VASIL'YEVA, S.F.,
provizor; FEL'DSHER, L.N., provizor; ZAKOSHANSKIT, N.Ya.,
red.

[Prepared druge; a manual for physicians] Gotovye lekarstvennye preparaty; spravochnik dlia vrachei. Moskva,
Meditsina, 1965. 228 p.

(MIRA 18:6)

CHARASTER CONTRACTOR STATES OF THE STATES

ISMAILOV, I.M., inzh.; GAVRILENKO, I.V., kand.tekhn.nauk; Prinimali uchastiye; KUTYAVIN, S.M.; ORESHKIN, D.K.; TADZHIBAYEV, G.T.; AKHUHDZHAHOV, A.I.; TOHKIKH, P.I.; PANCHENKO, A.I.; FEL! DSHER, M.G.; VORONINA, L.D.

Lowering the solvent content in seed meal before treatment in evaporators. Mabl.-zhir.prom. 26 no.10:7-13 0 '60. (MIRA 13:10)

l. Vsesoyuznyy nauchno-issledovatel skiy institut zhirov (for Ismailov, Gavrilenko). 2. Uch-Kurganskiy masloekatraksionyy zavod (for Kutyavin, Oreshkin, Tadzhibayev). 3. Sredneaziatskiy filial Vsesoyuznogo nauchno-issledovatel skogo instituta zhirov (for Panchenko, Felidsher, Voronina). (Uch-Kurgan--Oil industries--Equipment and supplies)

APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R0004128300

DRUZHININ, I.G.; VARFOLOMEYEVA, L.T.; FELIDSHER, S.A.

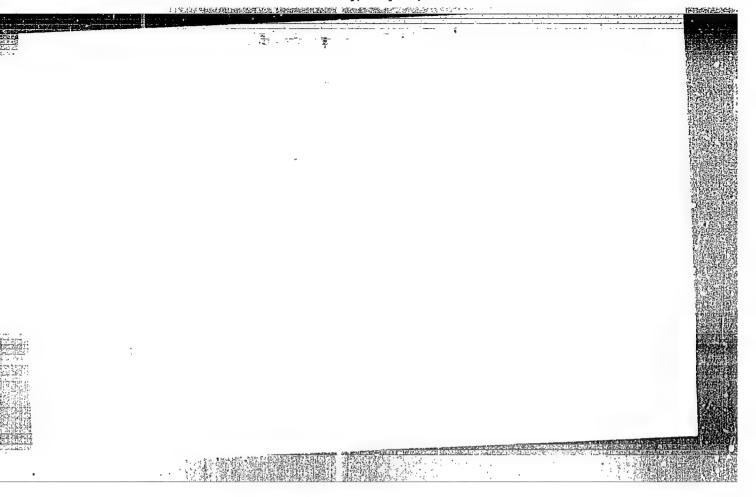
Comparative characteristics of the chemical composition of well waters on the "Vasil'evskii" State Farm. Uch. zap. Biol.-pochv. fak. Kir. um. no.7:155-162 *58. (MIRA 15:10) (Kirghizistan—Water—Composition)

APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R0004128300

MANT'YEV, V.A.; FEL'DSHEROV, I.A.

Analytical and micro-preparation apparatus for continuous paper electrophoresis. Vop. med. khim. 7 no.5:542-545 S-0 '61.

1. The Biochemical Laboratory of the P.A.Gertsen State Oncological Institute, Moscow.
(PAPER ELECTROPHORESIS -- EQUIPMENT AND SUPPLIES)



Our motto is mass participation! Voen. znam. 40 mo.4:42
Ap '64. ("TRA 17:6)

1. Zamestitel' predsedatelya fabrichnogo komiteta Vsesoyuznogo dobrovol'nogo obshchestva sodeystviya armii, aviatsii i flotu SSSR po sportivnoy rabote, Kiyev.

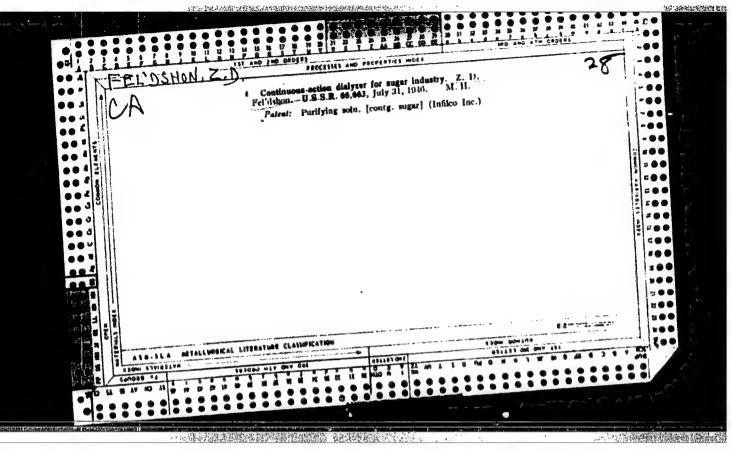
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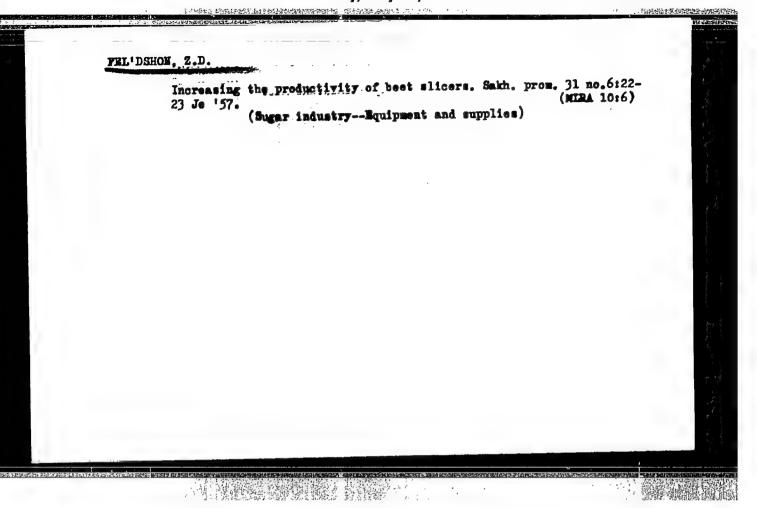
GRIGOR'YEV, V. [Hryhor"iev, V.]; FEL'DSHON, Z., kand.tekhn.nauk; GINDIS, Ya. [Hindis, IA.], inzh.; AKININ, P., inzh.

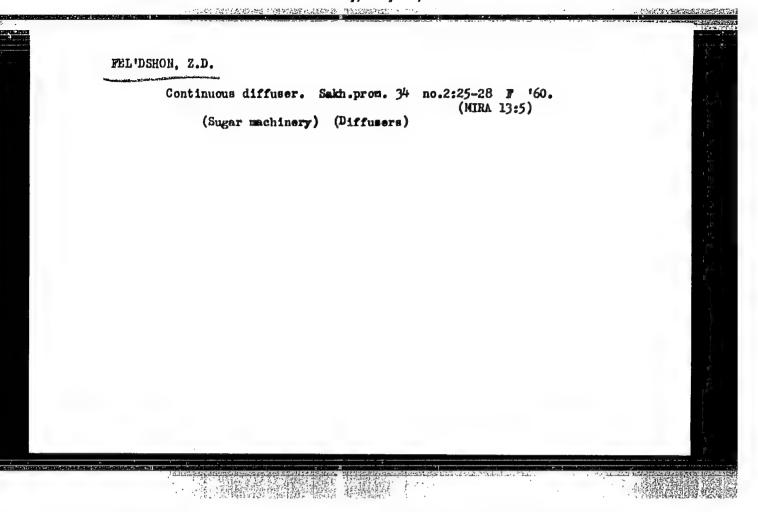
Automation of the production of slag "pumice" on a centrifugal machine. Bud.mat.i konstr. no.5:22-25 S-0 '62. (MIRA 15:11)

l. Deystvitel'nyy chlen Akademii stroitel'stva i arkhitektury UkrSSR (for Grigor'yev).

(Automation control) (Slag)







BRAND, V.M.; GRUTMAN, M.S. [Hrutman, M.S.]; FEL'DERION, Z.D.; POLTGRATSKAYA,
Ye. [Poltorate'ka, R.], red.; IOAKIMIS, A., tekhn.red.

[Reed in rural construction] Komysh v sil'a'komu budivnytetvi.

Kytv. Dersh.vyd-vo lit-ry s budivnytetva i arkhitektury URSS.,
1959. 122 p.

(Reed (Botany)) (Farm buildings)

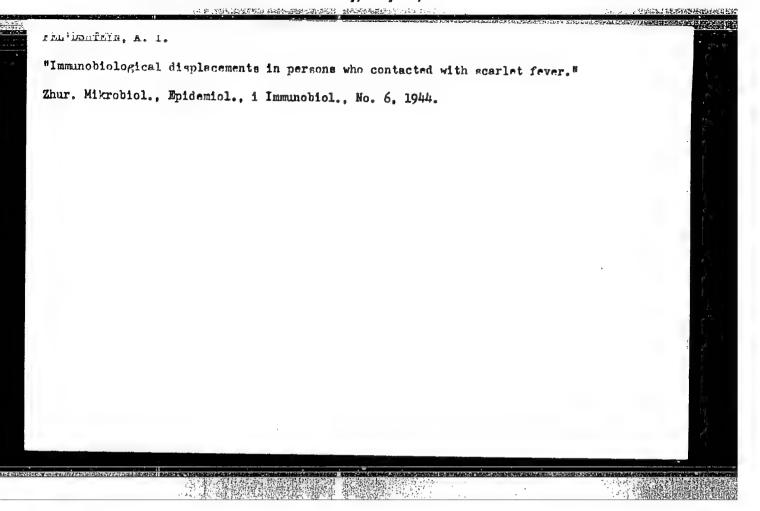
FEL! DSHTEYN, A.G.

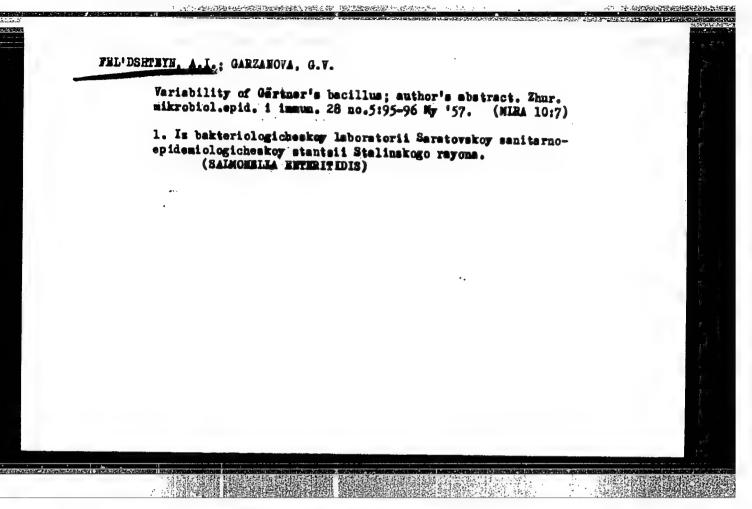
On the treatment of hypertension. Sovet.med. no.4:30-31 Apr 51. (CLML 20:8)

1. Candidate Medical Sciences Fel'dshteyn. 2. Odessa.

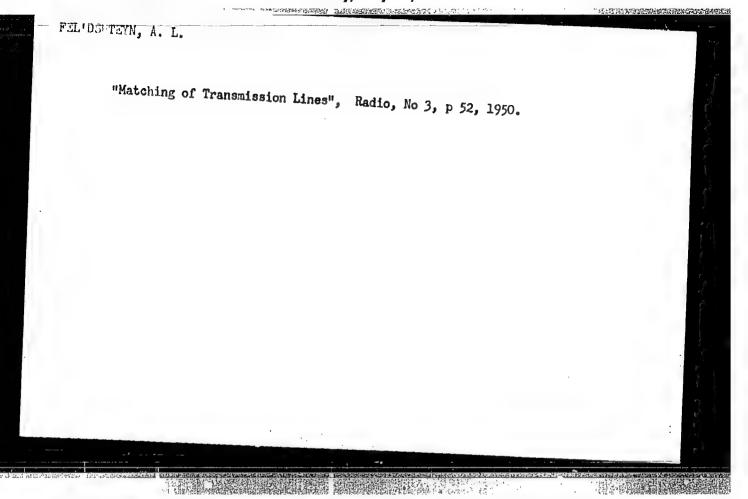
"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000412830





ea 1/50157 FELIDSHTEYE, A. L. USER/Engineering - Transmission Lines Jul/Ang 49 Radio - Transmission Lines "Energy Relations in a High-Frequency Transmission Line," A. L. Fel'dshteyn, Engr, 5 pp "Radiotekh" Vol IV, No 4 Discusses energy relations in a long line with lesses for a fixed set of conditions at the terminus and starting point. Examines the conditions for optimal energy relations in treating the generator-line load system as a closed space. Introduces the concept of "operating quality" of such a system and the areas of application of this concept. Submitted 17 Mar 49. 1/50737



Radiophysics, Application of Radiophysics Methods
Radiotekhnika, Vol 6, No 5, 1951. "Nomuniform (Communications) Lines."

No abstract.

S0: Radiotekhnika, Vol 9, No 2, Mar/Apr 54; 64-30785, 28 July 1954)

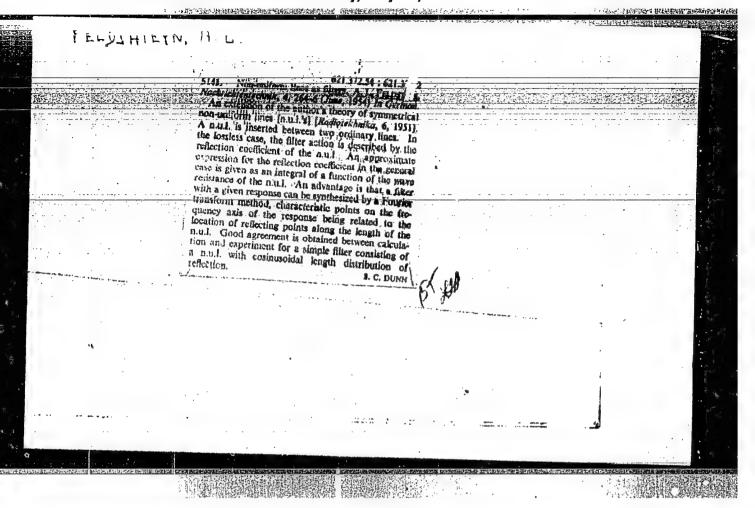
Radiophysics, Application of Radiophysics Methods
Radiotekhnika, Vol 7, No 6, 1952. "Synthesis of Nomuniform (Communications) Lines."

No abstract.

SO: Radiotekhnika, Vol 9, No 2, Mar/Apr 54; (W-30785, 28 July 1954)

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000412830



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AUTHORS:

Fel'dshteyn, A. L., of the Society

Member

SOV/108-13-8-3/12

TITLE:

Some Problems in the Synthesis of Heterogenesus Lines (Neketoryye

zadachi sinteza neodnorodnykh liniy)

PERIODICAL:

Radiotekhnika, 1958, Vol. 13, Nr 8, pp. 13 - 23 (USSR)

ABSTRACT:

The author describes the method of the synthesis by means of the Laplace integral and gives examples for the construction. of heterogeneous lines according to given frequency characteristics. The approximation formula (10) of (Ref 1) serves as a basis for the calculation. This reference shows the connection between the line structure and the reflection factor at the line terminal: formula (1). The function-given by formula (4) - which characterizes the relative change of the characteristic impedance is introduced and formula (1) is written down in the form of the transform according to Laplace-Karson (?)(Karson) as formula (5). The function F(p) occurring in it denotes the reflection factor and therefore can already previously be subjected to the limitations restricting the circuit functions that can be physically realized (Ref 2). These limitations are for the reflection factor the following: 1) $|F(p)| \le 1$ on the axis of real

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Some Problems in the Synthesis of Heterogeneous Lines SOV/108-13-8-3/12

frequencies. 2) F(p), besides the poles in the left semi-plane of the complex variable p does not have any other special points. The meromorphous function F(p) is then written down in form of a quotient of two integral functions and the final form for the equation; (1) is obtained: formula (6). This integral equation has a general solution in form of the so-called expansion formula by Heaviside (Khevisayd):formulæ (7) or (6). Examples are given. They show the use of the formulæ (7) or (6). The examples can be divided into two groups: 1) The demanded frequency characteristic is given. 2) The equivalent circuit diagram LCR is given which is to be investigated. There are 14 figures and 4 references, 3

SUBMITTED:

August 8, 1957

1. Frequency 2. Mathematics 3. Electric circuits

Card 2/2

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SOV/109---4-3-25/38

AUTHORS: Fel'dshteyn, A.L., Yavich, L.R.

TITLE: A Comparison of Step-like and Continuous Line Sections (K sravneniyu stupenchatykh i plavnykh perekhodov)

PERIODICAL: Radiotekhnika i Elektronika, Vol 4, Nr 3, 1959, pp 527-529 (USSR)

ABSTRACT: First, a Chebyshev-type step-like section (see Fig 1) is considered. This device was investigated by a number of authors (Refs 2,5,6 and 8). It is assumed that the length of this type of line section, which consists of n small steps is given by:

 $\ell_0 = \frac{1}{2\pi} \Lambda_2 \text{ n arc } \cos \left\{ \frac{1}{\cos \frac{K}{n}} \right\}$ (1)

where Λ_2 is the wavelength in the transmission line corresponding to the "long-wave" boundary of the transmission range; K is expressed by Eq (2), where R is the ratio between the characteristic impedances of the matched lines; h is the maximum deviation of the Chebyshev polynomial from its zero value. When n in Eq (1) tends to infinity, the line section represents a continuous transition, and Eq (1) is in the form of

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SOV/109---4-3-25/38

Eq (3). The problem consists of comparing values of as given by Eqs (1) and (3), for the same value of R and the same value of the reflection coefficient. The results are shown in Fig 4 for various values of n and [7; the limiting case of a continuous transition is represented by the dashed curves. There are 5 figures and 8 references, 6 of which are translated from English. One of the Soviet references is SUBMITTED: September 18. 1958

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S/109/60/005/05/006/021 E140/E435

AUTHORS:

Fel'dshteyn, A.L. and Yavich, L.R.

TITLE:

The Calculation of Stepped Junctions with Maximally-

Flat Characteristics

PERIODICAL: Radiotekhnika i elektronika, 1960, Vol 5, Nr 5,

pp 762-770 (USSR)

ABSTRACT:

A method is given for calculating two- and three-step waveguide junctions with maximally-flat characteristics. Tables are given for wave-impedance changes between 1.2 and 9.2. Acknowledgements are expressed to R.Sh.Sharikova for her assistance with the calculation There are 9 figures, 2 tables and 3 Soviet

references.

SUBMITTED:

April 13, 1959

Card 1/1

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77175 SOV/108-15-1-1/13

AUTHOR:

Fel'dshteyn, A. L., Yavich, L. R.

TITLE:

Engineering Computation of Chebyshev's Stepped

Transitions

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PERIODICAL:

Radiotekhnika, 1960, Vol 15, Nr 1, pp 3-15 (USSR)

ABSTRACT:

The paper is an exposition of the method of engineering computation of the method of engineering computation of stepped transitions between transmission lines. The results of calculation of 405 typical problems are given in table form. The following two basic definitions are given: (1) A stepped transition is a quadrupole consisting of n sections of the transmission line (steps") which have the same length $\mathcal L$ and various wave impedances ρ_i (see Fig. 1).



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Fig. 1.

Engineering Computation of Chebyshev's Stepped Transitions

77175 SOV/108-15-1-1/13

The purpose of a stepped transition is to match two lines with the wave impedances $\hat{\rho}$ and r, respectively. (2) A stepped transition is called optimal, or Chebyshev, when (a) for a selected wave impedance jump $R=r\hat{\rho}_0$, (b) a selected permissible mismatching value is $/\Gamma/_{\rm max}$, and (c) for a selected passband $\lambda_2 - \lambda_1$, the transition has a minimum overall length $\ell_0 = n \, \ell$. The attenuation of a Chebyshev transition equals 10 \log_{10} of the magnitude $/T_{11}/^2$, which is:

$$|T_{11}|^2 = 1 + h^2 T_n^2 \left(\frac{\cos \theta}{\rho}\right) = 1 + h^2 T_n^2(x),$$
(1)

Card 2/6

where $T_{11}(x)$ is the Chebyshev polynomial of the first type and n-th order, n=1, 2, 3... being the

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Engineering Computation of Chebyshev's Stepped Transitions

77175 SOV/108-15-1-1/13

number of transition steps; h is a parameter defining the permissible mismatch $/\Gamma/_{max}$; p is

a parameter defining the width of the passband; $\Theta = 2\pi \mathcal{Q}/\Lambda$ is electrical length of the step and Λ is the wavelength in the transmission line. The stepped transitions are usually characterized by 5 parameters: n, h, p, R and \mathcal{L}_0 , of which 3

may be selected independently of each other whereas the two others follow from computation. The relationship between these parameters is derived from Eq. (1) by considering $\cos \Theta = 1$, i.e., for zero length of the steps, and taking values of the argument $x = \cos \Theta/p$ at the boundaries of the passband. The following expressions have been obtained:

 $p = \frac{1}{\cos\left(\frac{1}{n}\arccos C\right)}.$ (12)

Card 3/5

Engineering Computation of Chebyshev's Stepped Transitions

$$\Lambda_1 = \frac{2\pi I}{\pi - \arccos \rho}.\tag{15}$$

$$\Lambda_{\mathbf{z}} = \frac{2\pi I}{\mathsf{arc}\cos\rho} \,. \tag{16}$$

where Λ_1 and Λ_2 are the wavelengths in the transmission line, generally different from λ_1 and λ_2 in the outside space. The length \mathcal{L}_o = n \mathcal{L} is given as:

$$\frac{I_0}{\Lambda_2} = \frac{1}{2\pi} n \arccos \left\{ \frac{1}{\cos \frac{1}{n} \arccos C} \right\}, \tag{18}$$

C in Eq. (18) and (12) is defined as:

Card 4/4

APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R0004128300

Engineering Computation of Chebyshev's Stepped Transitions

77175 SOV/108-15-1-1/13

 $C = \frac{R-1}{2h\sqrt{R}} .$

Expressions are given for the wave impedances ρ_1 of the steps of transitions with n=2, n=3, and n=4. Values of R, p, and ρ_1 are given in tables for n=2, n=3, and n=4, and for various magnitudes of $\left| \Gamma \right|_{\text{max}}$. The tables give the solution of 405 typical synthesis problems of stepped transitions. Two numerical examples illustrate the use of the tables for rapid computation of similar problems. In an appendix to the paper, expressions for ρ_1 and ρ_2 in a two-step transition are derived by comparing the coefficients of $\cos \Theta$ in Eq. (1) and in an attenuation equation obtained as a product of matrices of stepped transition elements. R. Shakirova helped make the calculations.

Card 5/5

9.1400 (2703,3803,1006)

S/108/60/015/006/007/012/XX B010/B070

AUTHOR:

Fel'dshteyn, A. L., Member of the Society

TITLE:

Generalized Matrix Theory of Inhomogeneous Lines

PERIODICAL:

Radiotekhnika, 1960, Vol. 15, No. 6, pp. 10-17

Systems of equations are given for the calculation of the elements of the transmission matrix of an inhomogeneous line. These equations appear promising for the unification of the methods of solving problems in line theory. It is assumed that the inhomogeneous line may be approximated by connecting numerous discreet passive four-poles in series. The transmission matrix (T) is, then, obtained as the product of the transmission matrices $(T)_t$ of the individual discreet four-poles. The following recurrence formulas hold for the elements (A_k, B_k, C_k, D_k)

of the total matrix:

 $A_k = \prod_{i=1}^k a_i + \sum_{m=1}^k b_m c_{m-1} \prod_{i=m+1}^k a_i$

Card 1/5

APPROVED FOR RELEASE: Monday, July 31, 2000

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Generalized Matrix Theory of Inhomogeneous

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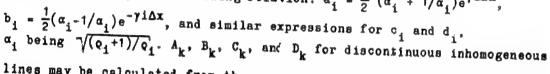
$$C_{k} = \sum_{m=1}^{k} c_{m} A_{m-1} \prod_{i=m+1}^{k}$$

$$B_k = \sum_{m=1}^k b_m D_{m-1}$$

 $C_{k} = \sum_{m=1}^{k} c_{m} A_{m-1} \prod_{i=m+1}^{k} d_{i}, \quad B_{k} = \sum_{m=1}^{k} b_{m} D_{m-1} \prod_{i=m+1}^{k} a_{i}, \quad D_{k} = \prod_{i=1}^{k} d_{i} + \sum_{m=1}^{k} c_{m} B_{m-1}$

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where a, b, c, and d are the matrix elements of the discreet four-poles, and k is their number. It is known that the wave transmission matrix ai, bi, ci, di of a section of line with wave impedance qi and length Ax adjoining another section with the wave impedance ϱ_{i+1} is given in the usual notation by the following relation: $a_i = \frac{1}{2} (\alpha_i^{1+1} / \alpha_i^{1}) e^{\gamma i \Delta x}$



lines may be calculated from the same expressions. For continuous inhomogeneous lines, that is, when the number of discreet four-poles becomes infinitely great, the sums and products go over into integrals:

Card 2/5

Generalized Matrix Theory of Inhomogeneous Lines

S/108/60/015/006/007/012/XX B010/B070

$$A(1) = \exp(\int_{0}^{1} \gamma(x)dx) + \int_{0}^{1} N(x)C(x)\exp(\int_{x}^{1} \gamma(x)dx)dx,$$

$$C(1) = \int_{0}^{1} N(x)A(x)exp(-\int_{x}^{1} \gamma(x)dx)dx, D(1) = exp(-\int_{0}^{1} \gamma(x)dx) + \int_{0}^{1} N(x)B(x)$$

$$\exp\left(-\int_{x}^{1} \gamma(x)dx\right)dx, B(1) = \int_{0}^{1} N(x)D(x)\exp\left(\int_{x}^{1} \gamma(x)dx\right)dx, \text{ where } N(x) = \frac{1d}{2dx} \ln_{Q}(x),$$

l is the length of the line; and A, B, C, D are elements of the transmission matrix. It is shown that these equations can be transformed, by the separation of variables, into four Volterra integral equations of the second degree which are known to yield well-converging series for the solution; also the error is easily estimated. The first approximation

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Generalized Matrix Theory of Inhomogeneous Lines

S/108/60/015/006/007/012/XX B010/B070

$$A_1 = \exp(\int_0^1 \gamma(x)dx), B_1 = \exp(-\int_0^1 \gamma(x)dx) \int_0^1 N(x)\exp(2\int_x^1 \gamma(x)dx)dx, \text{ and cor-}$$

responding expressions for C_1 and D_1 ; the magnitudes of the errors involved are given by $\triangle A \le (\text{ch Ml})-1$, $\triangle B \le (\text{sh Ml})$ - Ml, and corresponding expressions for AC and AD, where M = Max |N(x)| (0 $\leq x \leq 1$). In some special cases, not dealt with in the paper, exact solutions may be obtained by solving the differential equations resulting from differentiating the integral equations with respect to the upper limit:

 $A'' - (N'/N)A' - \left\{ (\gamma^2 + N^2) + (\gamma' - \gamma N'/N) \right\} A = 0, C'' - (N'/N)C' - \left\{ (\gamma^2 + N^2) - (\gamma' - \gamma N'/N) \right\} C = 0, B'' - (N'/N)B' - \left\{ (\gamma^2 + N^2) + (\gamma' - \gamma N'/N) \right\} B = 0,$ $D'' - (N'/N)D' - \{(\gamma^2 + N^2) - (\gamma' - \gamma N'/N)\}D = 0, \text{ where A, B, C, D are the}$ transmission matrix elements, and the primed quantities are differential coefficients with respect to 1. In conclusion, it is indicated that the

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Generalized Matrix Theory of Inhomogeneous Lines

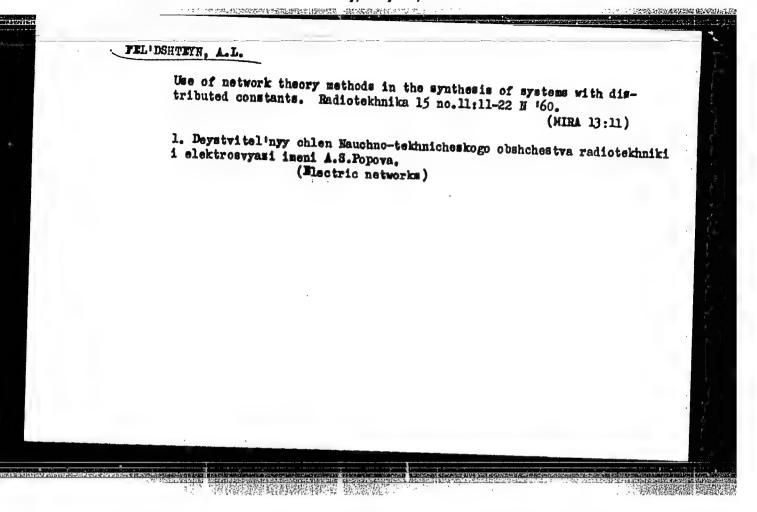
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difficult calculation of the input reflection coefficient may be simplified with the help of Riccati's differential equation combined with the solutions of the four integral or differential equations. There are 4 figures and 12 Soviet references.

SUBMITTED: December 17, 1958

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Card 5/5



9,1900 (a1502603)

20577 5/109/61/006/002/009/023 E140/E435

AUTHOR:

Fel'dshteyn, A.L.

TITLE:

The Synthesis of Step Directional Couplers

PERIODICAL: Radiotekhnika i elektronika, 1961, Vol.6, No.2,

pp.234-240

TEXT: The author starts from the well-known directional coupling properties of coupled homogeneous transmission lines. Relationships are developed for two special cases: 1) directional couplers with minimum number of sections (Chebyshev or isoextremal characteristics); 2) coupler with maximally-smooth characteristics. The author also considers the question of the physically attainable properties of directional systems. proceeds from the single-step directional coupler (homogeneous symmetrical coupled lines), multi-step directional coupler (cascade connection of arbitrary number of homogeneous coupled lines) and the limiting case of the multi-step system (inhomogeneous coupled It is found that the last case presents an infinite passband dropping to zero only at zero frequency. of power between the branches has a polynomial character, permitting the design of directional couplers with similar

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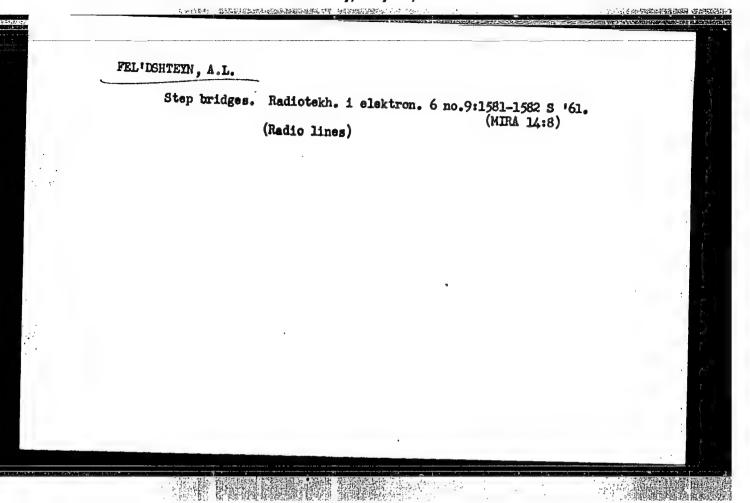
The Synthesis of Step ...

S/109/61/006/002/009/023 E140/E435

properties to those of step tapers and step filters. Certain mathematical demonstrations are included in an appendix. There are 6 figures, 1 table and 9 references: 8 Soviet and 1 English.

SUBMITTED: June 9, 1960

Card 2/2



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22728

S/108/61/016/005/002/005 B104/B205

9,14.00 AUTHOR:

Fel'dshteyn, A. L., Member of the Scientific and Technical Society of Radio Engineering and Electric Communications imeni A. S. Popov

TITLE:

Non-uniform coupled lines

PERIODICAL: Radiotekhnika, v. 16, no. 5, 1961, 7. - 14

TEXT: It is first noted that there are no data available in the literature on the theory of non-uniform coupled lines, which offers new possibilities for the synthesis of optimum superhigh-frequency eight-terminal networks. In presenting this theory, the author proceeds from a network consisting of s cascade-connected eight-terminal networks which he considers to be composed of two eight-terminal networks, i.e., the s-th eight-terminal network and the system of the preceding (s-1) eight-terminal networks. Therefore, the transmission matrix of the entire system may be represented as the product of the transmission matrix of the s-th eight-terminal network and that of the system of (s-1) eight-terminal networks. Based on these assumptions, the author obtains four systems of equations describing the network of s eight-terminal networks with

22728

Non-uniform coupled lines

S/108/61/016/005/002/005 B104/B205

discretely varying parameters. Next, a network is studied, in which each eight-terminal network is considered to be a pair of symmetric homogeneous lines (Fig. 2). The cascade connection of these lines is regarded as a coupled line of several stages (Fig. 3). Current and voltage in homogeneous, coupled lines are known to be given by the system

$$U_{1} = U_{8} \cos ml + j \left(\rho I_{8} + rI_{4} \right) \sin ml$$

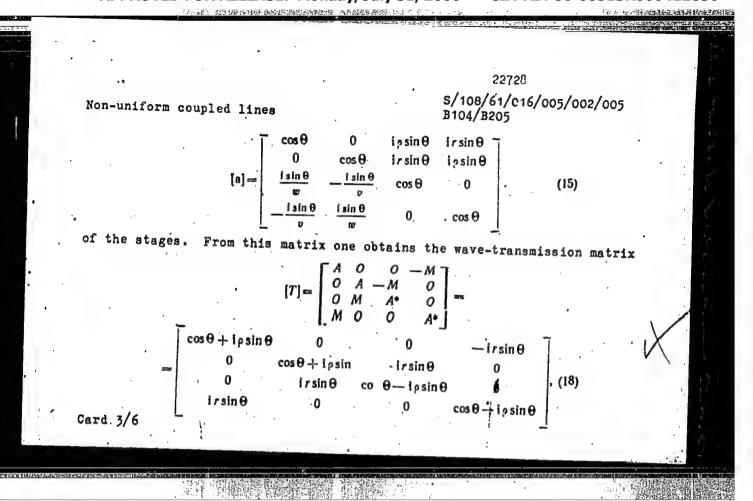
$$U_{2} = U_{4} \cos ml + j \left(rI_{8} + \rho I_{4} \right) \sin ml$$

$$I_{1} = I_{8} \cos ml + j \left(\frac{U_{8}}{w} - \frac{U_{4}}{v} \right) \sin ml$$

$$I_{2} = I_{4} \cos ml + j \left(\frac{U_{4}}{w} - \frac{U_{9}}{v} \right) \sin ml$$
(13)

where q and w stand for the characteristic impedance, and r and v for the coupling impedance. The coefficients of Eqs. (13) form the matrix

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Non-uniform coupled lines

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of the stages on the assumption that all lines in the eight-terminal network have the same characteristic impedance $(\rho_1 = \rho_2 = \rho_3 = \rho_4 = R)$ and the condition $rv = R^2$ is satisfied. Here, $r \sim r/R$ and $r \sim r/R$ are normalized. This system is fully determined by the two elements A and M, for which the following relations are derived by passing to a limit. In this procedure, the entire system is conserved and the number of stages is infinitely increased:

 $A(1) = \exp(im \int_{0}^{1} (x) dx) - \inf_{x \to \infty} r(x) M(x) \exp(im \int_{0}^{1} (x) dx) dx$ (22)

 $M(1) = \lim_{x \to \infty} r(x)A(x)\exp(-i\pi \int_{x}^{x} (x)dx)dx$ (23)

Thus, non-uniform coupled lines with balanced current and voltage coupling are fully determined by two integral equations similar to those obtained for non-uniform single lines. The successive approximation of Eqs. (22) and design problems are discussed finally. It is shown that of the four parameters (0, w, r, v) of coupled double conductors, only two parameters, e.g., o and r, are independent. An additional coupling,

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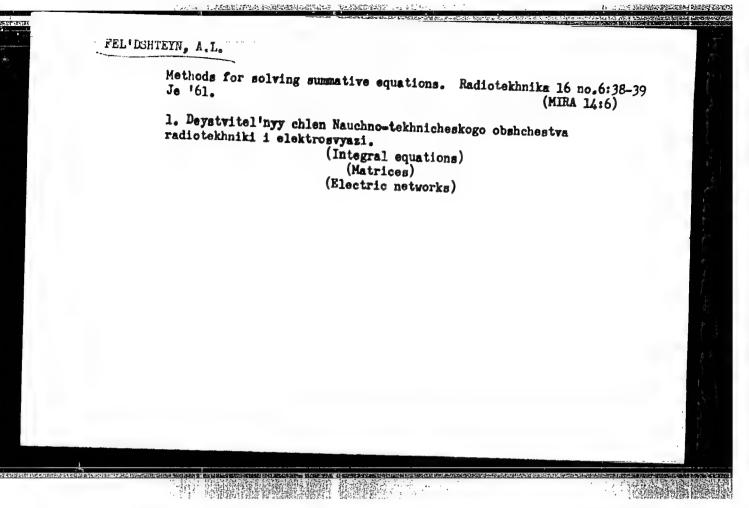
Non-uniform coupled lines

S/108/61/016/005/002/005 B104/B205

rv = R^2 = 1, exists in the case under consideration (Fig. 4). Hence, only one of the four parameters is independent, e. g., r(x) which is then given by the relation $r(x) = 60 \ln \left\{ 1 + \left(\frac{D}{a_{12}} \right)^2 \right\}$. It is shown that, if the coupling impedance in this form can be changed by a change of D, the relation $\rho(x) = \sqrt{1+r^2(x)} = 120 \ln \frac{D}{a}$ will be obtained only by varying the diameter a of the conductor. If r(x) is obtained by varying a_{12} , then the corresponding change of $\rho(x)$ will be brought about through a variation of D or a. Similar results are obtained for lines with coaxial or plane coupling. There are 4 figures and 6 Soviet-bloc references.

SUBMITTED: October 10, 1960

Card 5/6



33778

S/108/62/01/1/001/005/007 D271/D304

9,1300

AUTHORS:

Fel'dshteyn, A.L., and Zhavoronkova, Ye.S., Members

of the Society (see Association)

TITLE:

Calculating the Chebyshev directional couplers, with

loose coupling

PERIODICAL: Radiotekhnika, v. 17, no. 1, 1962, 40 - 50

TEXT: A synthesis method is presented for multi-element optimal directional couplers, and design data are tabulated for couplers consisting of 2 - 11 elements. The coupler which is considered is shown in Fig. 2; its function is to branch a required power from the main line 1-3 into 4, while the leak into 2 remains below the permitted limit. Transfer coefficients S₁₂ and S₁₄ are functions of frequency; if they are of Chebyshev (iso-thermal) character, a minimum number of elements is required. Elements of the coupler are

minimum number of elements is required. Elements of the coupler are four-port networks as shown in Fig. 3, where a is the number of the element. Scatter matrices of the coupler and of its elements are of the type

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S/108/62/017/001/005/007
Calculating the Chebyshev directional ... D271/D304

$$[S] = \begin{bmatrix} S_{11}S_{12} & S_{12}S_{14} \\ S_{12}S_{11} & S_{14}S_{12} \\ S_{12}S_{14} & S_{12}S_{12} \\ S_{12}S_{14} & S_{12}S_{12} \end{bmatrix} \times [S]_{\bullet} = \begin{bmatrix} S_{11}^{\bullet} & S_{12}^{\bullet} & S_{12}^{\bullet} & S_{14}^{\bullet} \\ S_{12}^{\bullet} & S_{11}^{\bullet} & S_{12}^{\bullet} & S_{13}^{\bullet} & S_{12}^{\bullet} \\ S_{13}^{\bullet} & S_{12}^{\bullet} & S_{12}^{\bullet} & S_{11}^{\bullet} \end{bmatrix}$$

$$(1)$$

Wave transfer matrix $[T]_{\alpha}$, assuming S_{11} , S_{13} , $S_{14} \ll 1$ and $S_{12} \cong 1$, is

$$[T]_{a} = \begin{bmatrix} e^{i\phi} & -S_{14}^{a} e^{i\phi} & -S_{11}^{a} & -S_{12}^{a} \\ -S_{14}^{a} e^{i\phi} & e^{i\phi} & -S_{12}^{a} & -S_{11}^{a} \\ -S_{12}^{a} & e^{i\phi} & S_{14}^{a} e^{-i\phi} \end{bmatrix},$$

$$[T]_{a} = \begin{bmatrix} e^{i\phi} & -S_{14}^{a} e^{i\phi} & -S_{12}^{a} & -S_{11}^{a} \\ -S_{12}^{a} & S_{11}^{a} & -S_{12}^{a} & -S_{14}^{a} e^{-i\phi} \end{bmatrix},$$

$$[T]_{a} = \begin{bmatrix} e^{i\phi} & -S_{14}^{a} e^{i\phi} & -S_{11}^{a} \\ -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \\ -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \end{bmatrix},$$

$$[S]_{a} = \begin{bmatrix} e^{i\phi} & -S_{14}^{a} e^{i\phi} & -S_{12}^{a} \\ -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \\ -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \end{bmatrix},$$

$$[S]_{a} = \begin{bmatrix} e^{i\phi} & -S_{14}^{a} e^{i\phi} & -S_{12}^{a} \\ -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \\ -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \end{bmatrix},$$

$$[S]_{a} = \begin{bmatrix} e^{i\phi} & -S_{14}^{a} e^{i\phi} & -S_{12}^{a} \\ -S_{12}^{a} & -S_{12}^{a} -S_{12}^{a} & -S_{12}^{a} & -S_{12}^{a} \\ -S_{12}^{a}$$

where $\theta = \frac{2\Im 1}{\Delta}$. Transfer coefficients are then written out as Card $2/8\gamma$

Calculating the Chebyshev directional... D271/D304

$$s_{11} = e^{-i\theta} \sum_{\alpha=1}^{n} s_{11}^{\alpha} e^{-i2(n-\alpha)\theta}, (9) \quad s_{13} = \prod_{q=1}^{n} s_{13}^{\alpha} e^{-i\theta} \approx e^{-in\theta}. (11)$$

$$S_{12} = e^{-i\theta} \sum_{\alpha=1}^{n} S_{12}^{\alpha} e^{-i2(n-\alpha)\theta}, (10) S_{14} = e^{-in\theta} \sum_{\alpha=1}^{n} S_{14}^{\alpha}, (12)$$

where each parameter of the coupler depends only on element parameters of the same designation. A particular case is considered when an element of the coupler is non-directional; because of symmetry

$$-S_{11}^{\alpha} = S_{12}^{\alpha} = S_{14}^{\alpha} = iC_{\alpha}$$
 (13)

where 10 log $\frac{1}{c_{\alpha}^2}$ is transfer attenuation of one dement. Transfer coefficients S_{12} and S_{14} become

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Calculating the Chebyshev directional... S/108/62/017/001/005/007

$$S_{12} = \sum_{\alpha=1}^{n} C_{\alpha} e^{-i2(n-\alpha)\theta}$$
 (14)

$$S_{14} = \sum_{\alpha=1}^{n} C_{\alpha}$$
 (15)

The entire system is then fully determined by values of C_{α} , S_{12} is a Fourier series which may be transformed into Chebyshev polynomials the maximum value of S_{12} is equal to S_{14} ; S_{14} is independent of frequency if C_{α} does not depend on frequency. This last property permits one to optimize the entire system by bringing only S_{12} into the form of Chebyshev polynomial. Expressions are obtained from (14) for various values of n_{12} , n_{12} , n_{13} , n_{14} , n_{14

 $S_{12} = (2C_1\cos 3\theta + 2C_2\cos \theta)e^{-i3\theta}$, $(C_1 = C_4; C_2 = C_3)$. (19)

Calculating the Chebyshev directional... D271/D304

It is postulated that backward transfer coefficient determined by expressions as above must have Chebyshev frequency characteristics:

$$\left| \mathbf{S}_{12} \right|_{\mathbf{n}} = \mathbf{h} \mathbf{T}_{\mathbf{n}-1} \left(\frac{\cos \theta}{\mathbf{p}} \right), \tag{21}$$

where h and p are amplitude and scale coefficients, $T_{n-1}(\Omega)$ - Chebyshev polynomial of first class and (n-1)order; h represents permitted value of S_{12} in the coupler pass-band. The obtainable value of p is

$$p = \frac{1}{\operatorname{ch}\left[\frac{1}{n-1} \text{ ar ch } \sqrt{\overline{k}}\right]}, \qquad (24)$$

where k is the minimum prescribed directivity; $k = |S_{14}|^2/h^2$. When p is known, the required number of elements can be found from

$$n = \frac{\operatorname{ar} \operatorname{ch} V\overline{k}}{\operatorname{ar} \operatorname{ch} \frac{1}{p}} + 1. \tag{25}$$

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Calculating the Chebyshev directional... S/108/62/017/001/005/007

In design work it is not p which is of interest but the working range $\Delta = 2 \frac{\lambda_2 - \lambda_1}{\lambda_2 + \lambda_1}$ and overlap coefficient $\chi = \lambda_2/\lambda_1$, which are obtained from p. In order to determine transfer coefficients of elements C_1 , C_2 , etc., Chebyshev polynomials are transformed into a form similar to that of the expression (19), e.g.

$$T_4(\frac{\cos\theta}{p}) = \frac{1}{p^4}\cos 4\theta + 4(\frac{1}{p^4} - \frac{1}{p^2})\cos 2\theta + (\frac{3}{p^4} - \frac{4}{p^2} + 1).$$
 (32)

By comparing expressions of the type (19) and (32) values of C_n/h are obtained as a function of p. These are tabulated (in dB) in design tables. Diameters of coupling holes are determined for the case of a coupler formed by two identical waveguides coupled by circular holes in the common short wall. For loose coupling, the expression relating transfer attenuation to dimensions of the hole is

Card 6/8/
$$L_{dB} = 20 \log \frac{1}{C_1} = 20 \log \frac{12 b}{\pi \Lambda} (\frac{a}{d})^3$$
. (34)

Calculating the Chebyshev directional... S/108/62/017/001/005/007

A numerical example is given illustrating the application of the method. Design data are presented in 10 tables giving values for n = 2, 3, ... 11 and p = 0.1, 0.2, ..., 1.0. There are 6 figures, 10 tables and 10 references: 5 Soviet-bloc and 5 non-Soviet-bloc. The 4 most recent references to the English-language publications read as follows: W.R. Hewlett, U.S.A. patent specification 2,871,452 of 3 January 27, 1959; E. Hensperger, The microwave journal, issue 2, no. 8, 1959; B. Levy, Proc. I.E.E., part C, no. 337E, 1959; J. Reed and ques. MTT-4, no. 4, 1956.

ASSOCIATION:

Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi im. A.S. Popova (Scientific and Technical Society of Radio Engineering and Electrical Communications imeni A.S. Popov) [Abstractor's note: Name of association taken from first page of journal]

SUBMITTED:

October 26, 1960

Card 7/87

FEL'DSHTEYN, Aleksandr L'vovich; YAVICH, Lev Rafaelovich; SAIRHOV,
Vitally Petrovich; PERETS, R.I., red.; BUL'DYAYEV, N.A.,
tekhn. red.

[Manual on the elements of waveguide technology] Spravochnik po elementam volnovodnoi tekhniki. Moskva, Gosenergoizdat, 1963. 359 p. (MIRA 17:2)

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FEL'DSHTEYN, A.L.; SMIRNOV, V.P.

Characteristic impedance of a rectangular wave guide. Radiotekhnika 18 no.4:78 Ap 163. (MIRA 16:5)

1. Deystvitel'nyy chlen Nauchno-tekhnicheskogo obshchestva radiotekhniki i elektrosvyazi imeni Popova. (Wave guides)

ACCESSION NR: AP3001124

\$/0108/63/018/006/0015/0025

AUTHOR: Mazepova, O. I.; Fel'dshteyn, A. L.; Yavich, L. R. Members of the Society

TITLE: Engineering calculation of SHF band-pass filters

SOURCE: Radiotekhnika, v. 18, no. 6, 1963, 15-25

TOPIC TAGS: SHF band-pass filter

ABSTRACT: The method of SHF filter calculation is based on an equivalent replacing of the lumped-parameter systems (low-pass filters and ladder-type band-pass filters) with the filters formed by inhomogeneities in waveguides. The article offers: (1) a systematic procedure for calculating SHF filters with quarter-wave couplings; (2) tabulated typical calculations. Functions of effective attentuation for both the Tchebycheff and the maximum-flat-frequency response filters are evaluated. Cavity resonators are represented by waveguide stubs terminated with three inductive posts on each end. The design tables were compiled by means of an electronic computer. "Programing was performed by Engineer A. V. Ivakina." Orig. art. has:

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ACCESSION NR: AP3001124

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi im A. S. Popova (Scientific and Technical Society of Radio Engineering and Electro-communications)

SUBMITTED: 07 Aug62

DATE ACQD: 01Jul63

ENCL: 00

SUB CODE: CO,SD

NO REF SOV: 002

OTHER: 006

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APPROVED FOR RELEASE: Monday, July 31, 2000

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ACCESSION NR: AP4042891

S/0108/64/019/007/0033/0038

AUTHOR: Fel'dshteyn, A. L. (Active member)

TITLE: Nonreciprocal nonuniform lines

SOURCE: Radiotekhnika, v. 19, no. 7, 1964, 33-38

TOPIC TAGS: nonuniform line, nonreciprocal line, nonreciprocal line theory

ABSTRACT: A long line with continuously varying (in the direction of propagation) nonreciprocal parameters is called a "nonreciprocal nonuniform line." In such a line, the attenuation and phase shift depend on the direction of transmission (ferrite, plasma, etc.). By considering the line as a ladder of quadripoles and by separating the reciprocal part from the nonreciprocal in each section, a theory of such lines is developed. The reciprocal part of a section is characterized by the half-sum of the conventional propagation constants $\partial_{r}(x)$ and $\nabla_{r}(x)$, while the nonreciprocal part is characterized by their half-difference. The integrals of

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ACCESSION NR: AP4042891

these quantities enter the formulas describing the line. Integral and differential formulas for the matrices of transmission and dissipation of the line are developed. "The author wishes to thank V. G. Kalina for discussing the results of the work." Orig. art. has: 1 figure and 30 formulas.

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi (Scientific and Technical Society of Radio Engineering and Electrocommunication)

SUBMITTED: 07Feb63

ENCL: 00

SUB CODE: EC

NO REF 50V: 004

OTHER: 000

Card 2/2

CIA-RDP86-00513R000412830

FZLIDSHTYN. Aleksandr Livovich; YAVICH, Lev Rafnelovich. Frinimala ichaetiye PROKHOROVA, N.I.; YAKORSON, A.Kh.

[Synthesis of four-terminal and eight-terminal microwave networks] Sintez chetyrekhpoliusnikov i vosimipoliusnikov na SVCh. Moskva, Izd-vo "Sviazi," 1965. 352 p.

(MIRA 18:5)

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Fel'dshteyn, Aleksandr L'vovi	ch; YAvich, Lev Rafael	lovich		60
Synthesis-high frequency four chetyrekhpolyusnikov i vo 352 p. illus., biblio. 5	terminal and eight-te		"Svyaz",	B+1 1965.
TOPIC TAGS: communication ne cation, transmission line	twork, array synthesis, waveguide coupler	, superhigh frequ	ency, SHF c	ommuni-
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Ch. IV. Cascade connections of four-termi	· ·	
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Ch. VI. Stepped transitions 120		K
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SUB CODE: 09/ SUBM DATE: 09Apr65/ ORIGI	REF: 080/ OTH REF: 033	

KUNIN, V.M., red.; FEL'DSHTEYN, A.M., red.

[Manufacture and use of arbolite] Proizvodstvo i primenenie arbolita. Moskva, 1962. 50 p. (MIRA 1776)

1, Giprosel'stroy.

	GINZBURG-RAKHMILEVICH, Sh.G.; FEL'DSHTEYN, A.S. kandidat meditsinskikh m	
	1. Chetvertaya infektsionnaya bol'nitsa Saratova.	(Dysentery)
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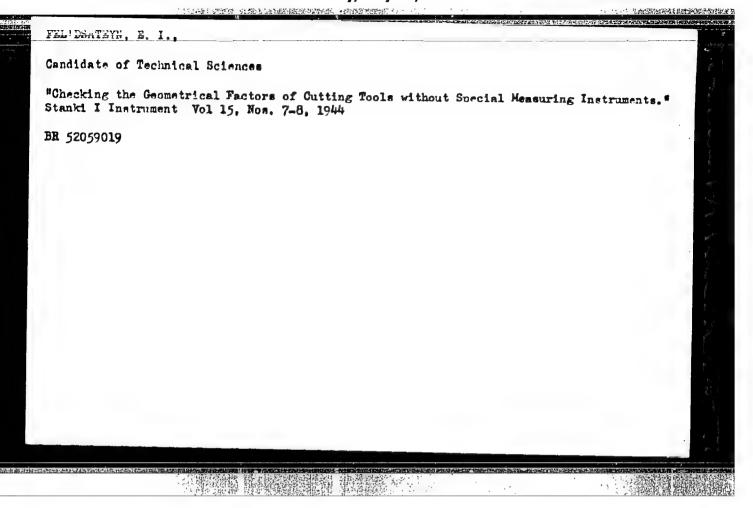
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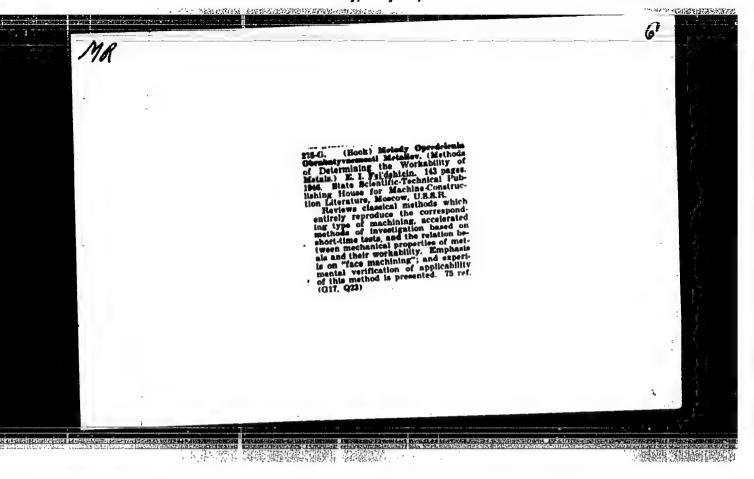
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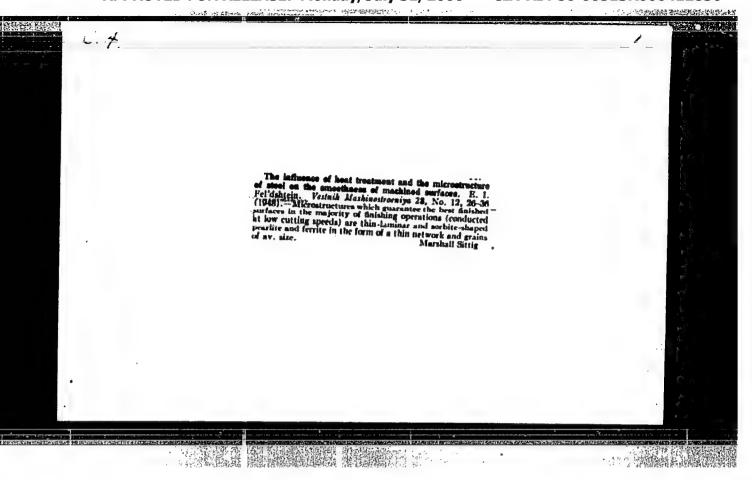
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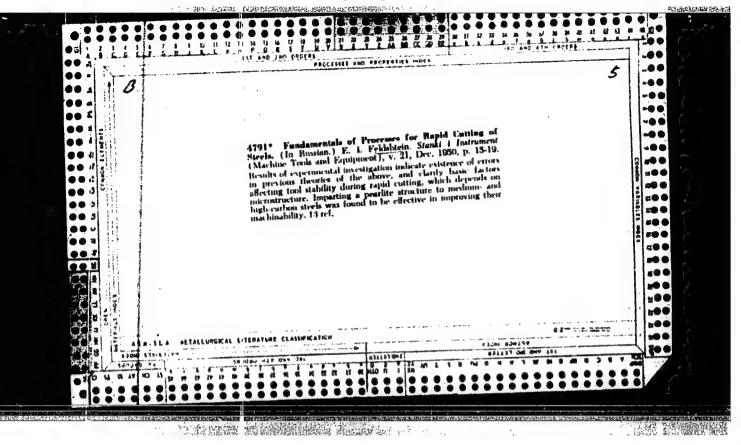
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2000 [19] 10 TELLINIZIE, E.L. PHATE I TREASURE ISLAND FIBLIOGRAPHICAL REPORT AID 482-I * B00% Call No.: AF639671 Authors: BASOV, M. I., Kand. of Tech. Sci., FEL'DSHTEYN, E. I., Kand. of Tech. Sci., BRAKHMAN, L. A., Eng., STITE YEV, YA. F., Ing., KRYSINA, YM. V., Tng., BOL'SHAKOV, V. M., Tech., BYCHKOV, P.P., Eng., BAPYLOV, G. I. Full Title: CUTTING TOOLS WITH HARD-ALLOY MULTIPLE BLADE I SERTS Transliterated Title: Rezhushchiye instrumenty a mnogolezmiynymi vstavkami iz tverdogo splava PUBLISHING DATA Originating Agency: None Publishing House: State Scientific and Technical Publishing House of Machine-Building Literature (Meshgiz) Date: 1952 No. pp.: 110 No of copies: 8,000 E ditorial Staff Editor: Basov, M. I., Kand. of Tech. Sci. TEXT DATA Coverage: This monograph is the collective work of authors from the Institute of the Or enization of the Automobile Industry, the Gor'kiy Automobile Plant im. Molotov (ZIM) and the Moscow Automobile Plant im. Stalin (ZIS). The authors describe the designs of modern cuttingtools with land-alloy multiple blade inserts, the results of their study and experience with he toold! cutting properties, and the adventieges of

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Ch. III Operation of Tools with Hard-Alloy Multiple	
Blade Insorts	80–89
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Pozhushchiye instrumenty a maogole: viynymi AID 482-I vstrykemi iz tverdogo snleve PAGES E vocaience in Industrial Use of Tools with Herd-Ch. IV Alloy Multiple Blade Inserts 90-102 Ch. V Efficiency of Use of Tools with Hard-Alloy Multiple Blade Inserts 103-109 (Efficiency of use of: E) cutters with prismatic inserts; 2) ZIM cutters with inserted plates; 3) Face milling cutters with cylindrical inserts; Increased efficiency of tools with hollow inserts) The book is intended for engineers, techniciens and Stakhano-Purpose: vites in machine-building plents. Facilities: "Organization of the Automobile Industry) Institute; ZIN (Gor'kiy Automobile Plant im. Moletov); ZIS (Moscow Automobile Plant im. Stalin) No. of Russian and Slavic References: None Available: A.I.D., Library of Congress

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: L- 2-31 ETT, Y-1. PHASE I TREASURE ISLAND BIBLIOGRAPHICAL REPORT AID 443 - I BOOK Call No.: TN731.F4 Author: FEL'DSHTEYN, E. I., Rand. of Tech. Sci. Full Title: MACHINABILITY OF STEELS IN CONNECTION WITH THE CONDITIONS OF HEAT TREATMENT AND WITH THE MICROSTRUCTURE Obrabatyvayemost' staley v svyazi s usloviyami Transliterated Title: termicheskoy obrabotki i mikrostrukturoy Publishing Data Originating Agency: None Publishing House: State Scientific and Technical Publishing House of Literature on Mechanical Engineering and Shipbuilding ("Mashgiz") Date: 1953 No. pp.: 255 No. of copies: 4.000 Editorial Staff Editor: Klushin, M. I., Kand. of Tech. Sci. Appraiser: Granovskii, G. I., Prof., Dr. of Tech. Sci. The author dedicates this work to the staff of the Gor'kiy Automobile Plant im. V. M. Molotov and expresses his thanks to M. I. Klushin and Ya. F. Stigneyev, supervisors in the Laboratory of Metal Cutting, and to engineers and technicians in machine shops of this plant. Text Data Coverage: This book is the result of the author's ten-year investigations of the machinability of structural and tool steels in relation

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to the conditions of heat treatment and to the microstructure. These

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investigations include the studies of the three basic factors of machinability: cutting speed, cleanness of finished surfaces and cutting pressure. Since the machinability of metals is not an abstract problem, it requires for its solution a wide range of experimental data. The main task of the author was not a simple gathering of information, but the establishment of general laws controlling these data, and their use for the practical needs of the industry. A specific feature of these investigations is the fact that they have been checked in industrial conditions. The author maintains that the correctness of the conclusions and their importance for the industry were proved by numerous tests and observations in machine shops of the Gor'kiy Automobile Plant.

Names of Russian scholars (since 1870) and of Soviet scientists (during the Stalin Five-Year Plans and in the postwar years), and discussions of their valuable contributions in this field are scattered through the book. Foreign scientists, particularly American and English, are mentioned with sharp criticism of their theories (e.g., p. 49-50). The book is provided with detailed descriptions of various kinds of steels, many illustrations of their microstructure and of the cleanness and roughness of surfaces, diagrams, temperature curves, numerous tables, sketches of machine elements, etc. The

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